

Aeroelasticity Research at Wright–Patterson Air Force Base (Wright Field) from 1953–1993

Terry M. Harris and Lawrence J. Huttshell

U.S. Air Force Research Laboratory, Wright–Patterson Air Force Base, Ohio 45433

Introduction

THE research and development facilities of Wright–Patterson Air Force Base (WPAFB, known earlier as Wright Field) have played a substantial part in the initiation, direction, development, and transfer of technologies related to flight vehicle aeroelasticity. The connection between WPAFB and aeroelasticity research began in the 1920s and has continued into the 21st century. This paper is not intended to be an inclusive review of the history of developments in aeroelasticity. The historical reviews by Garrick and Reed,¹ Bisplinghoff,² and Collar³ are excellent accounts of developments in aeroelasticity. Early encounters with problems of static aeroelasticity, flutter, and dynamic loads are also documented in the book by Flomenhoft.⁴ The WPAFB-sponsored research contributed significantly to advancements in aeroelasticity, and an attempt is made herein to summarize this research.

Pre-1953

Work in prediction and prevention of aeroelastic instabilities was being accomplished in the 1920s at McCook Field, Dayton, Ohio, the predecessor of WPAFB.^{5,6} By the late 1930s a Flutter and Vibrations Section had been established within the Aircraft Laboratory at what was then known as Wright Field.⁶ This office was active through the WWII years and beyond in a hands-on approach to assisting the aircraft manufacturers with the many flutter and vibration problems starting to occur in higher-performance aircraft. Much of the aeroelastic testing in these early years had to be done in flight because the authorities that controlled wind-tunnel operation would not permit the testing of

flexible models that ran the risk of damaging the tunnels upon breakup.⁷

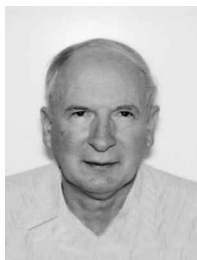
One of the most important products of this team was the 1942 in-house technical report by Lt. Ben Smilg and Lee Wasserman commonly known as “4798,” that is, “Application of Three-Dimensional Flutter Theory to Aircraft Structures.”⁸ This report provided nondimensional aerodynamic coefficients as functions of reduced frequency and were tabulated for various values of commonly used flutter parameters. The employment of these tables greatly decreased the labor and time required for flutter computations. “4798” helped transition the theory of Theodorsen, Garrick, and Kussner into production-line engineering analysis methods needed to prevent flutter. Industry used the tables extensively, expanded the method to include modal degrees of freedom, and employed the report as a manual to train new aeroelasticians. The application of the 4798 method significantly reduced the occurrences of aileron, elevator, and rudder flutter problems. Tab flutter analysis was addressed in another in-house report.⁹ This report contained elaborate tables of aerodynamic coefficients for control surfaces and, again, was used widely in the aircraft industry. Cases addressed included spring-controlled tabs, geared tabs, and trim tabs. “5153” was particularly timely and useful in determining the causes and remedies for the rash of spring tab flutter cases that occurred in the late 1940s and early 1950s.

The 1950s

The late 1940s and 1950s saw the de facto training by the Flutter and Vibrations Section of many of the nationally known aeroelasticians. [Raymond L. Bisplinghoff, the distinguished authority and



Terry M. Harris is the Chief of the Design and Analysis Methods Branch, Structures Division, Air Vehicles Directorate, Air Force Research Laboratory at Wright–Patterson AFB, Ohio. He received a B.S. in aeronautical and astronautical engineering from Purdue University in 1972 and an M.S. in aerospace engineering from the University of Dayton in 1979. As an engineer in the Directorate’s Design and Analysis Group in the 1970s and the Aeroelasticity Group in the 1980s, Mr. Harris gained considerable experience in aeroelasticity and aeroservoelasticity. He was the Air Force program manager for numerous programs for the development of flutter optimization methods and wind tunnel tests involving active and adaptive flutter suppression for aircraft carrying external stores. As Leader of the Aeroelasticity Group from 1987 to 1997, Mr. Harris oversaw the development of many aspects of aeroelasticity-related technologies. Mr. Harris has authored or coauthored over thirty publications, including seven national and international conference papers and two *Journal of Aircraft* articles. He is a Senior Member of AIAA.



Lawrence J. Huttshell is the Aeroelasticity Team Leader in the Design and Analysis Methods Branch, Structures Division, Air Vehicles Directorate, Air Force Research Laboratory at Wright–Patterson AFB, Ohio. He received a B.S. in mechanical engineering from the University of Louisville in 1967 and an M.S. in aeronautical and astronautical engineering from the Ohio State University in 1972. Mr. Huttshell has considerable experience in unsteady aerodynamic, aeroelasticity, and aeroservoelasticity. He has led several national and international programs: unsteady pressure measurement programs with the Netherlands, active flutter suppression wind tunnel tests (Germany, France, England, and Israel) and a USAF/German flight test demonstration, and a joint AF/NASA NASP government work package for panel flutter. He has served on Executive Independent Review Teams and consulted on system problems in the area of unsteady aerodynamics, aeroelasticity, buffet, and aeroservoelasticity. He is currently leading an in-house team for computational aeroelasticity. Mr. Huttshell has over 70 publications, eight of which are in archival journals. He is an Associate Fellow of AIAA.

educator in aeroelasticity, served as a consultant in the Wright Field Flutter and Vibrations Section in 1941–1943 (Ref. 2).] Ray Peloubet, for many years the leader of the General Dynamics, Fort Worth, Texas, structural dynamics team, spent his formative years in the Flutter and Vibrations Section, as did Henry Katz of the McDonnell Corporation, Leon Tolve of Lockheed, and Herb Voss of Boeing. Furthermore, at about this time Lee Wasserman departed U.S. Air Force service and formed his own flutter model design company, Dynamic Devices, in itself a valuable asset to aeroelasticity research for many years.¹⁰ Wasserman's flutter models and engineering support significantly helped in avoiding flutter and assuring flight safety.

During the 1950s, the Flutter and Vibrations Section sponsored a large number of wind-tunnel tests, especially in the investigation of transonic phenomena. These tests provided valuable research data needed to support the new systems in the absence of dependable analysis methods. 1952–1956 saw transonic flutter trends established by flutter model tests on a wide variety of wing planforms in investigations into the effects of sweep, aspect ratio, tip pods, and engine location. Flutter tests were also conducted to investigate control surface flutter and trim tab flutter. Results from this series of wind-tunnel tests were used in the design of the F-100, F-105, F-106, B-52, and B-58 (Cooley, D. E., "Major Milestones in Flutter Prevention Technology," unpublished document). In the period 1952–1960, all-moveable stabilizer flutter characteristics were established through model testing. (Transonic results are documented in Ref. 11.) Results were used in the design of the F-100, F-101, F-105, F-4, and C-141 (Cooley, D. E., "Major Milestones in Flutter Prevention Technology," unpublished document). This research originated as an in-house activity and continued as a contract with Bell Aircraft. Tests, and analyses specifically for T-tail flutter were run from 1952–1960; results were applied to the design of the Matador missile, F-104, C-141, DC-9, and Boeing 727 (Cooley, D. E., "Major Milestones in Flutter Prevention Technology," unpublished document).^{12,13}

In 1956, the Flutter and Vibrations Section sponsored a series of transonic flutter model tests with Cornell University for 45-deg swept wings, straight wings, and 60-deg delta wings.^{14–16} These tests provided a set of flutter data for a wide range of nondimensional flutter parameters, which formed a valuable database for aeroelastic design and analysis.

In the mid-1950s the loss of an F-101 fighter in an incident of panel flutter resulted in a series of investigations that continued through 1967. The objective of these efforts was to develop suitable prediction methods, to produce reliable and repeatable experimental data, and to develop design criteria.^{17,18}

The 1960s

The 1960s saw an emphasis on supersonic and hypersonic aeroelastic wind-tunnel testing—both for lifting surface flutter and for panel flutter—pushed by the need for technology development for the Dyna-Soar orbiting aerospace plane, the XB-70 supersonic bomber, and the X-24 lifting-body vehicles. In March of 1963, the WPAFB aeroelasticity research office became part of the newly established U.S. Air Force Flight Dynamics Laboratory (AFFDL). Much hypersonic research was accomplished through the AFFDL Project ASSET (Aerothermodynamic/elastic Structural Systems Environmental Tests), which employed Thor and Thor-Delta boosters to fire glide models down the Eastern Test Range.⁷ The ASSET gliders were flat-bottomed, 69-in. (1.7526 m) long test articles with 70-deg delta wings. Included in the major goals of ASSET were the obtaining of panel flutter data and oscillatory pressure data at high Mach numbers.

Unsteady aerodynamics research and design for aeroelastic prediction methods was a key research area throughout the 1960s.^{19–26} The importance of interference effects had been shown for T-tails. In 1966 subsonic flutter model tests by Boeing²⁷ showed the serious deficiency in the state of the art for configurations with variable sweep wings. One of the first experimental programs in the transonic regime was defined in 1966 by the AFFDL and was performed by the Cornell Aeronautical Laboratory.²⁸ In 1968 the AFFDL con-



Fig. 1 Subsonic wing-tail flutter model with various wing/tail positions.

ducted an in-house test program to further explain the mechanism of wing-tail flutter.^{29,30} The wind-tunnel model is shown in Fig. 1 with various wing/tail positions. These tests provided more complete trends with systematic variations of controlling parameters, defined flutter prevention criteria, and provided experimental data for code validation.

Also during these years, the AFFDL first began its development of finite element analytical methods, such as MAGIC,³¹ a displacement method approach developed through Bell Aerospace. Aeroelasticians became interested in the development of these programs when it was shown that the stiffness matrices generated, coupled with eigenvalue solvers and mass information, gave reasonable mode shape and frequency results that could be employed in flutter and dynamic response analyses.

The 1970s

During the 1970s, major improvements in linear unsteady aerodynamic prediction tools were made. Based on the success of the planar doublet-lattice code developed by Albano and Rodden,³² the AFFDL sponsored the development of a doublet-lattice code for nonplanar surfaces through the Douglas Corporation. The H7WC doublet-lattice code³³ was a preliminary version of the method, which accounted for body/lifting surface interference by direct application on nonplanar lifting surface elements, whereas N5KA,³⁴ the "final" version, used an image system and an axial singularity system to account for the effects of the body. However, demand for a viable unsteady aerodynamic tool was so great that the AFFDL distributed H7WC in advance of N5KA. By happenstance, H7WC became probably the most widely distributed unsteady aero code of all time and, further, was incorporated into structural analysis and design tools (FASTOP, NASTRAN, etc.). In the area of supersonic code development, the AFFDL sponsored through Boeing the development of an improved Mach Box code for nonplanar wings and wing-tail configurations.^{35,36}

There was a rapid development of numerical methods for computing aerodynamic forces for small-disturbance transonic flows about oscillating airfoils and planar wings. Based on the procedure first introduced for steady flows by Murman and Cole,³⁷ Traci et al. developed computer programs (STRANS and UTRANS)^{38,39} for two-dimensional small-disturbance steady and unsteady transonic flows about oscillating airfoils. The finite difference relaxation method was extended to oscillating planar wings^{40,41} and applied in a transonic flutter analysis of a rectangular wing in Ref. 42. During this period, Ballhaus and Goorjian⁴³ developed a computer code, LTRAN2, which solves the two-dimensional, nonlinear, low-frequency, small-disturbance transonic flow equation by an alternating-direction-implicit algorithm. This popular two-dimensional code was used by many investigators and improved for unsteady aerodynamic and aeroelastic applications. Some of the AFFDL-sponsored applications are discussed in Refs. 44–46.

Wind-tunnel testing was performed to validate the various unsteady aerodynamic prediction methods. The AFFDL and the U.S. Air Force Armament Test Laboratory sponsored unsteady aerodynamic testing of an F-5 wing model with and without external stores in the Dutch National Aerospace Laboratory (NLR) tunnel in Amsterdam.⁴⁷⁻⁵⁰ The store represented an AIM-9J missile and was successively mounted at the wing tip and on an underwing pylon. These test results quickly became an international standard for validation of the newly developing computational unsteady aerodynamic prediction methods.

Automated tools were being developed, which combined fully stressed strength design with other, namely, flutter, constraints. The AFFDL sponsored the development of FASTOP (Flutter and Strength Optimization Procedure)⁵¹ through the Grumman Aerospace Corporation in 1975. This program contained a doublet-lattice (subsonic) routine and a Mach-box (supersonic) routine for iterative, converging flutter and strength design of metallic structure. By 1978, FASTOP-3 (Ref. 52) was released, which extended the method to composite structure.

The application of advanced filamentary composites to aircraft structures in the 1960s, such as the proposed composite wing for the F-111 Transonic Improvement Program, later called TACT (Transonic Aircraft Technology) emphasized the need for automated preliminary design tools. The first method to address this need was tailoring and structural optimization (TSO), developed by General Dynamics under AFFDL sponsorship. TSO incorporated aeroelastic tailoring as its primary objective, that is, "the embodiment of directional stiffness into aircraft structural design to control aeroelastic deformation, static and dynamic, in such a fashion as to affect the aerodynamic and structural performance in a beneficial way."⁵³ The AFFDL sponsored numerous improvements to TSO and validated the program through several series of wind-tunnel tests and design studies extending into the early 1980s, both in-house and on contract.^{54,55}

At this time AFFDL aeroelasticians were participating in the TACT program and assisting in the design of the Highly Maneuverable Aircraft Technology (HiMAT). The HiMAT remotely piloted vehicle, built by Rockwell for testing at the NASA Dryden Research Center, Edwards, California, was the first modern aircraft to fly with aeroelastically tailored lifting surfaces.

A major application of aeroelastic tailoring was in the design of forward-swept wings, in which, for example, low divergence speeds could be eliminated through proper orientation of the wing's composite fibers. The design aspects of forward-swept wings were being addressed in house through analytical studies and wind-tunnel tests while the AFFDL oversaw for DARPA (Defense Advanced Research Projects Agency) feasibility studies with General Dynamics, Grumman, and Rockwell, followed by wind-tunnel demonstration programs conducted by Grumman⁵⁶ and Rockwell.⁵⁷ These investigations formed the confidence base for the X-29, a forward-swept wing fighter-size flight demonstrator (Fig. 2), the development of which was monitored for DARPA by an AFFDL advanced development program office in the 1980s. Aeroelastic tailoring and flutter optimization methods were used extensively in the design of the X-29 to preclude divergence and body-freedom flutter.

One of the most prevalent aeroelastic problems facing the U.S. Air Force over the years was the reduction in flutter speeds suffered by wings carrying external stores. During this period, the AFFDL attacked the problem of predicting wing/store flutter, with the knowledge that many aircraft (F-4, F-16, etc.) were capable of carrying many thousands of store combinations. With the Air Force Seek Eagle Office (responsible for stores clearance) as the primary customer, the AFFDL sponsored the development by Northrop of perturbation methods⁵⁸ and by McDonnell Douglas the computer code FACES (Flutter of Aircraft with External Stores).^{59,60} The perturbation technique was developed to expedite flutter clearance of many store combinations by rapidly screening out the major stores combinations in a typical stores flutter study. Significant flutter characteristics are singled out by the method, and relatively few new baseline analyses were needed to allow this perturbation study to complete the flutter trend in a new range. The FACES computer program was



Fig. 2 X-29 flight demonstrator aircraft.



Fig. 3 YF-17 flutter suppression model in the wind tunnel.

developed especially for simplified and efficient aircraft/external store flutter analyses.

Another approach to the wing-store flutter problem was through active flutter suppression, that is, the commanding of control surfaces, through a control law, to oscillate at a counteracting force and phase. The first of AFFDL's analytical investigations was with McDonnell Douglas, in which flutter suppression methods were applied to the F-4.⁶¹ Soon thereafter, the AFFDL commissioned Northrop with the design of a wing-store flutter suppression system for a half-span, wall-mounted model of the YF-17 fighter shown in Fig. 3. The model was built by Dynamic Devices and was used in a long series of experiments in the NASA Langley Research Center's 16-ft Transonic Dynamic Tunnel (TDT).^{62,63} The YF-17 international flutter suppression wind-tunnel test program sponsored by the AFFDL involved the development of control laws and verification testing, again in the NASA Langley TDT. Under this international cooperative program, MBB (Messerschmitt-Bölkow-Blohm) under German sponsorship, the French ONERA (Office Nationale d'Etudes et de Recherches Aérospatiales), the Israeli Technion Institute under a NASA grant, Northrop Corporation under AFFDL contract, British Aerospace under Royal Aeronautical Establishment sponsorship, and in-house AFFDL researchers designed and evaluated control laws for testing.⁶⁴ The control laws for active suppression of an explosive wing-store flutter case were tested in October 1979. Results were very promising and demonstrated substantial potential for this technology.

Other active flutter suppression contracts were awarded to Rockwell International for developing control laws for the HiMAT unmanned vehicle⁶⁵ and to General Dynamics to develop flutter suppression methods for the F-16.⁶⁶ The first American flight test (Fig. 4) of active flutter suppression occurred earlier when the



Fig. 4 B-52 CCV flight-test aircraft.

AFFDL sponsored the implementation of such a system during the B-52 control-configured-vehicle (CCV) flight tests.^{67,68}

Adverse aeroelastic interaction with the flight vehicle control system led the U.S. Air Force to perform research in the prevention of these aeroservoelastic instabilities.⁶⁹ The AFFDL sponsored a number of efforts with McDonnell Douglas⁷⁰ and General Dynamics⁷¹ in an effort to find efficient ways to predict and prevent these occurrences. In-house efforts to achieve a viable, efficient aeroservoelasticity (ASE) prediction tool for both analog and digital control systems continued into the 1980s.⁷²

1980–1993

By the early 1980s, the research arm of the U.S. Air Force was called by then AFWAL (Air Force Wright Aeronautical Laboratories), and, as of October 1988, it was called WRDC (Wright Research and Development Center). As just described the AFFDL portion of AFWAL was performing in-house validation tests of aeroelastic tailoring techniques and wind-tunnel tests of forward-swept wing designs, in parallel with the X-29 development.^{73,74} The X-29 demonstrator brought together the following advanced technologies: forward-swept wing, close-coupled canard, aeroelastic tailoring, advanced structures and composites, relaxed static stability, fly-by-wire digital flight control, and advanced integrated subsystems.

In January 1980 the AFFDL portion of AFWAL was redesignated the Flight Dynamics Laboratory (FDL). In that year another international effort in flutter suppression reached its culmination. The FDL, with McDonnell Douglas as its contract support, in cooperation with the German Ministry of Defense designed and implemented a flutter suppression system that was flight tested on a German Air Force F-4F (Fig. 5) with external stores.⁷⁵

In the early 1980s the FDL continued its development of flutter suppression techniques, through Northrop and the YF-17 model, and through General Dynamics employing a quarter-scale, full-span, cable-flying F-16 model designed for testing in the Langley TDT (Fig. 6). By the mid-1980s the FDL changed its emphasis in active flutter suppression to adaptive flutter suppression, that is, control laws that would automatically adjust themselves for changing flight condition and store configuration. Northrop Corporation again was contracted to design a flutter control system for the YF-17 model.^{76,77} During the related series of tests, a wing-tip store was released, which resulted in a low flutter speed configuration. The control system detected the changed dynamics and implemented a new control law that successfully suppressed the flutter response. Later that decade General Dynamics was contracted for a series of adaptive flutter suppression investigations for their F-16 wind-tunnel model. These developments culminated in the testing of a near fully adaptive flutter suppression system for the F-16 model.⁷⁸

In addition to ASE instabilities and active flutter suppression research, a third area of investigation into control system/aeroelastic



Fig. 5 F-4 active flutter suppression flight-test aircraft.



Fig. 6 F-16 flutter suppression model in the wind tunnel.

interaction started in the early 1980s and continues today. On the basis of a Rockwell International proposal to the FDL, the active-aeroelastic-wing (AAW, at the time called active flexible wing) concept was developed and wind tunnel tested in the NASA Langley TDT. This concept employs multiple control surfaces as tabs, using the power of the airstream to shape the wing to achieve the desired effect, such as improved roll rates or efficient cruise. Several contracted investigations, plus tests on a subsonic wind-tunnel model designed and fabricated by FDL aeroelasticians and based on the F-16 Agile Falcon,⁷⁹ showed total aircraft takeoff weight, depending on configuration, could be reduced substantially using this technology. AAW technology was shown to be so promising that the FDL initiated a flight demonstration program with Boeing implementing the concept on a modified F/A-18.⁸⁰

Throughout this later period the FDL (later called the Flight Dynamics Directorate) researchers were concerned with investigating ways to predict and control buffeting of the twin tails of fighter-type aircraft at high angles of attack and of preventing damage caused by this phenomenon. The FDL sponsored investigations in the 1980s and 1990s, including numerous wind-tunnel tests^{81,82} to obtain buffet data. The eventual goal will be a flight demonstration of active suppression systems actuating either the existing rudders or piezoelectric panels integral to the skin of the vertical tails (or both concepts combined).

Another area of investigation involved large amounts of wind-tunnel testing under a joint effort with NASA. This program included the design, fabrication, and test of NASP (National Aerospace Plane) components. The FDL designed and sponsored the fabrication of both all-moveable wing/stabilator and vertical tail aeroelastic models,⁸³ and a panel flutter model.⁸⁴ The lifting surface models were tested in the NASA Langley TDT, and the panel flutter model was tested in the Unitary Tunnel at NASA Langley.

In the field of unsteady aerodynamics, the FDL sponsored numerous investigations involving the transonic small disturbance (TSD) theory. This research (1978–1982) resulted in the development by Boeing of the XTRAN3S computer code.⁸⁵ It was the first operational code to incorporate both the effects of unsteady flow and structural flexibility in a three-dimensional aerodynamic solution of a nonlinear potential equation, specifically the inviscid transonic modified small disturbance equation. XTRAN3S demonstrated the advantage of the TSD formulation in terms of relatively inexpensive computational cost, gridding simplicity, and the potential for realistic aircraft configurations.

Also during this time, the FDL sponsored a number of wind-tunnel tests to obtain unsteady pressure data for validating the new unsteady aerodynamic codes. Unsteady transonic pressure measurements were performed on a semispan model of a transport type supercritical wing, oscillating in pitch.⁸⁶ The tests of this Lockheed, Air Force, NLR, and NASA (LANN) model were conducted in the NLR wind-tunnel. In addition, the FDL and the Dutch Ministry of Defense sponsored a wind-tunnel program in 1992 to investigate the unsteady aerodynamic aspects of transonic high-incidence flows over a simple straked-wing model.^{87–90} The model was oscillated sinusoidally in pitch at various amplitudes and frequencies for mean angles of attack from 4 to 48 deg. In addition, maneuver-type transient motions of the model were tested. Both the LANN and simple straked-delta-wing models were tested in the NLR wind tunnel in Amsterdam. The data from both of these tests have been selected by Research and Technology Organization (formerly AGARD) as a standard for validating unsteady aerodynamic computations.⁹¹

The FDL went on to sponsor the Lockheed–Georgia Company in the development of the Euler/Navier–Stokes three-Dimensional Aeroelastic (ENS3DAE) method.^{92,93} ENS3DAE solves the full three-dimensional compressible Reynolds averaged Navier–Stokes equations, the thin-layer approximation to these equations or the Euler equations using an implicit approximate factorization algorithm. A linear generalized mode shape structural model is closely coupled with the aerodynamic method to analyze structurally flexible vehicles. A series of improvements has been made by Lockheed, the FDL, NASA Langley, and Georgia Tech to enhance the code's capabilities and computational efficiency.

Building upon the structural optimization codes of the 1970s, the FDL went on to sponsor through Northrop the development of the ASTROS (Aerospace Structural Optimization System) code.⁹⁴ This extensive program made use of the most modern programming methods of the time to provide for the design of air vehicle structures in the presence of static loads, aeroelastic, deflection, and buckling constraints. ASTROS has been independently judged as an excellent research tool and has been distributed to over 100 companies, universities, and laboratories.

Summary

In an effort to help solve existing problems and preclude future surprises, the research arm of the U.S. Air Force, housed at Wright–Patterson Air Force Base, has stood in the forefront of aeroelasticity research and design, through contracted and in-house investigations, “paper” studies, wind-tunnel experiments, and flight tests. The individuals involved in this research also contributed to the military specifications, safety reviews, and accident investigations. The research efforts flow beyond the 40-year span of this report and continue today. The organization (currently known as the Air Vehicles Directorate of the Air Force Research Laboratory, AFRL) serves as the office of primary responsibility in developing advanced technologies to predict and prevent adverse aeroelastic problems and in employing aeroelastic concepts to enhance future designs.

Acknowledgments

The authors wish to thank Dale E. Cooley and Michael H. Shirk—the “old hands” of the Aeroelasticity Section at Wright–Patterson Air Force Base—for their long memories, and especially Walter J. Mykytow, whose career in aeroelasticity at Wright–Patterson Air Force Base began in 1939 and extended (as a consultant) into the

1980s. Others with long memories who deserve our thanks include Ed Pendleton, Jim Olsen, Ken Griffin, and Max Blair.

References

- ¹Garrick, I. E., and Reed, W. H., “Historical Development of Aircraft Flutter,” *Journal of Aircraft*, Vol. 18, No. 11, 1981, pp. 897–912.
- ²Bisplinghoff, R. L., “History of Aeroelasticity,” *The Revolution in Structural Dynamics*, edited by H. I. Flomenhoft, Dynaflo Press, Palm Beach Gardens, FL, 1997, Chap. 1.
- ³Collar, A. R., “The First Fifty Years of Aeroelasticity,” *Aerospace*, Vol. 5, Feb. 1978, pp. 12–20.
- ⁴Flomenhoft, H. I., *The Revolution in Structural Dynamics*, Dynaflo Press, Palm Beach Gardens, FL, 1997.
- ⁵Gaffney, T., “The Forgotten Field—Dayton’s McCook Field,” *Dayton Daily News Article*, Vol. 107, No. 356, 31 Aug. 1984, p. 17.
- ⁶Pearson, J., and Henderson, D., “The Air Force Shock and Vibration Story,” *50 Years of Shock and Vibration Technology*, edited by H. C. Pusey, The Shock and Vibration Information Analysis Center, Booz-Allen and Hamilton, Inc., Arlington, VA, 1996.
- ⁷Many Contributors/Authors, “The Heritage of the Flight Dynamics Laboratory,” Flight Dynamics Lab., Dayton, OH, Oct. 1988.
- ⁸Smilg, B., and Wasserman, L., “Application of Three-Dimensional Flutter Theory to Aircraft Structures,” U.S. Army Air Forces, TR 4798, Materiel Center Wright Field, Dayton, OH, July 1942.
- ⁹Wasserman, L. S., Mykytow, W. J., and Spielberg, I. N., “Tab Flutter Theory and Applications,” Army Air Force, TR 5153, Wright Lab., Dayton, OH, Sept. 1944, Chap. 1.
- ¹⁰Liu, D. D., Sarhaddi, D., Piolenc, F. M., Wasserman, L. S., Roberts, W., Donham, R. E., Watts, G. A., and Peloubet, R. P., Jr., “Flutter Prevention Handbook: A Preliminary Collection,” Wright-Lab., WL-TR-96-3111, Dayton, OH, March 1997.
- ¹¹D’Ewart, B. B., Jr., and Farrell, R. F., “Transonic Flutter Characteristics of a 45 Degree Swept Back All Movable Stabilizer,” Wright Aeronautical Development Center, WADC TR-57-392, Dayton, OH, May 1958.
- ¹²Pengelly, C., Wilson, L., Epperson, T., and Ransleben, G., “Flutter Characteristics of a T-Tail,” Wright Aeronautical Development Center, TR 52-162, Dayton, OH, Nov. 1954.
- ¹³Wasserman, L., “Flutter Research of a T-Tail at Transonic Speeds,” Wright Aeronautical Development Center, TR 58-210, Dayton, OH, Dec. 1958.
- ¹⁴Maier, H. G., and King, S. R., “Transonic Flutter Model Tests: Part I—45 Degree Swept Wings,” Wright Aeronautical Development Center, WADC-TR-56-214, Dayton, OH, Sept. 1957.
- ¹⁵Brady, W. G., King, S. R., and Maier, H. G., “Transonic Flutter Model Tests: Part II—Straight Wings,” Wright Aeronautical Development Center, WADC-TR-56-214, Dayton, OH, Jan. 1958.
- ¹⁶Balcerak, J. C., and Ostaszewski, N. H., “Transonic Flutter Model Tests: Part III—60 Degree Delta Wings,” Wright Aeronautical Development Center, WADC-TR-56-214, Dayton, OH, Jan. 1958.
- ¹⁷Shirk, M. H., and Olsen, J. J., “Recent Panel Flutter Research and Applications,” AGARD, Rept. 475, Paris, France, Sept. 1963.
- ¹⁸Lemley, C. E., “Design Criteria for the Prevention of Panel Flutter,” Vols. I and II, Air Force Flight Dynamics Lab., AFFDL-TR-67-140, Dayton, OH, Aug. 1968.
- ¹⁹Vivian, H. T., and Andrew, L. V., “Unsteady Aerodynamics for Advanced Configurations Part I—Application of the Subsonic Kernel Function to Nonplanar Lifting Surfaces,” Flight Dynamics Lab., FDL-TDR-64-152, Dayton, OH, May 1964.
- ²⁰Rodemich, E. R., and Andrew, L. V., “Unsteady Aerodynamics for Advanced Configurations Part II—A Transonic Box Method for Planar Lifting Surfaces,” Flight Dynamics Lab., FDL-TDR-64-152, Dayton, OH, May 1964.
- ²¹Albano, E., and Andrew, L. V., “Unsteady Aerodynamics for Advanced Configurations Part III—Elliptic-Conical Wing in Linearized Unsteady Transonic Flow,” Flight Dynamics Lab., FDL-TDR-64-152, Dayton, OH, May 1964.
- ²²Moore, M. T., and Andrew, L. V., “Unsteady Aerodynamics for Advanced Configurations Part IV—Application of the Supersonic Mach Box Method to Intersecting Planar Lifting Surfaces,” Flight Dynamics Lab., FDL-TDR-64-152, Dayton, OH, May 1964.
- ²³Li, T. C., “Unsteady Aerodynamics for Advanced Configurations, Part V—Unsteady Potential Flow Around Slender Bodies at Angles of Attack,” Flight Dynamics Lab., FDL-TDR-64-152, Dayton, OH, May 1964.
- ²⁴Andrew, L. V., and Stenton, T. E., “Unsteady Aerodynamics for Advanced Configurations Part VII—Velocity Potentials in Non-Uniform Transonic Flow Over a Thin Wing,” Flight Dynamics Lab., FDL-TDR-64-152, Dayton, OH, Aug. 1965.

- ²⁵Stenton, T. E., and Andrew, L. V., "Transonic Unsteady Aerodynamics for Planar Wings with Trailing Edge Control Surfaces: Part I and Part II," Air Force Flight Dynamics Lab., AFFDL-TR-67-180, Dayton, OH, Aug. 1968.
- ²⁶Donato, V. W., and Huhn, C. R., "Supersonic Unsteady Aerodynamics for Wings with Trailing Edge Control Surfaces and Folded Tips," Air Force Flight Dynamics Lab., AFFDL-TR-68-30, Dayton, OH, Aug. 1968.
- ²⁷Topp, L. J., Rowe, W. S., and Shattuck, A. W., "Aeroelastic Considerations in the Design of Variable Sweep Airplanes," International Congress of the Aeronautical Sciences, Paper 66-12, London, 1966.
- ²⁸Balcerak, J. C., "Flutter Tests of Variable Sweep Configurations," Air Force Flight Dynamics Lab., AFFDL-TR-68-101, Dayton, OH, Sept. 1968.
- ²⁹Myktyow, W. J., Noll, T. E., Huttshell, L. J., and Shirk, M. H., "Subsonic Flutter Characteristics of a Variable Sweep Wing and Horizontal Tail Combination," Air Force Flight Dynamics Lab., AFFDL-TR-69-59, Dayton, OH, Nov. 1970.
- ³⁰Myktyow, W. J., Noll, T. E., Huttshell, L. J., and Shirk, M. H., "Investigation Concerning the Coupled Wing-Fuselage-Tail Flutter Phenomenon," *Journal of Aircraft*, Vol. 9, No. 1, 1972, pp. 48-54.
- ³¹Jordan, S., and Mallet, R., "MAGIC—An Automated General-Purpose System for Structural Analysis," Vol. I, Theoretical Manual, Air Force Flight Dynamics Lab., AFFDL-TR-68-65, Dayton, OH, July 1969.
- ³²Albano, E., and Rodden, W. P., "A Doublet Lattice Method for Calculating Lift Distribution on Oscillating Surfaces in Subsonic Flows," *AIAA Journal*, Vol. 7, No. 2, 1969, pp. 279-285.
- ³³Giesing, J. P., Kalman, T. P., and Rodden, W. P., "Subsonic Unsteady Aerodynamics for General Configurations: Part I, Vol. I—Direct Application of the Nonplanar Doublet-Lattice Method; Part I, Vol. II—Computer Program H7WC," Air Force Flight Dynamics Lab., AFFDL-TR-71-5, Dayton, OH, Nov. 1971.
- ³⁴Giesing, J. P., Kalman, T. P., and Rodden, W. P., "Subsonic Unsteady Aerodynamics for General Configurations: Part II, Vol. I—Application of the Doublet-Lattice Method and the Method of Images to Lifting-Surface/Body Interference; Part II, Vol. II—Computer Program N5KA," Air Force Flight Dynamics Lab., AFFDL-TR-71-5, Dayton, OH, April 1972.
- ³⁵Ii, J. M., Borland, C. J., and Hogley, J. R., "Prediction of Unsteady Aerodynamic Loadings of Non-Planar Wings and Wing-Tail Configurations in Supersonic Flow, Part I—Theoretical Development, Program Usage, and Application," Air Force Flight Dynamics Lab., AFFDL-TR-71-108, Dayton, OH, March 1972.
- ³⁶Kramer, G. D., and Keylon, G. E., "Prediction of Unsteady Aerodynamic Loadings of Non-Planar Wings and Wing-Tail Configurations in Supersonic Flow, Part II—Computer Program Description," Air Force Flight Dynamics Lab., AFFDL-TR-71-108, Dayton, OH, March 1972.
- ³⁷Murman, E. M., and Cole, J. D., "Calculation of Plane Steady Transonic Flows," *AIAA Journal*, Vol. 9, No. 1, 1971, pp. 114-121.
- ³⁸Traci, R. M., Albano, E. D., Farr, J. L., and Cheng, H. K., "Small Disturbance Transonic Flows About Oscillating Airfoils," Air Force Flight Dynamics Lab., AFFDL-TR-74-37, Dayton, OH, June 1974.
- ³⁹Farr, J. L., Traci, R. M., and Albano, E. D., "Computer Programs for Calculating Small Disturbance Transonic Flows About Oscillating Airfoils," Air Force Flight Dynamics Lab., AFFDL-TR-74-135, Dayton, OH, Nov. 1974.
- ⁴⁰Traci, R. M., Albano, E. D., and Farr, J. L., "Small Disturbance Transonic Flows About Oscillating Airfoils and Planar Wings," Air Force Flight Dynamics Lab., AFFDL-TR-75-100, Dayton, OH, Aug. 1975.
- ⁴¹Farr, J. L., Traci, R. M., and Albano, E. D., "Computer Programs for Calculating Small Disturbance Transonic Flows About Oscillating Planar Wings," Air Force Flight Dynamics Lab., AFFDL-TR-75-103, Dayton, OH, Aug. 1975.
- ⁴²Eastep, F. E., and Olsen, J. J., "Transonic Flutter Analysis of a Rectangular Wing with Conventional Airfoil Sections," *AIAA Journal*, Vol. 10, No. 10, 1980, pp. 1159-1164.
- ⁴³Ballhaus, W. F., and Goorjian, P. M., "Implicit Finite-Difference Computations of Unsteady Transonic Flows About Airfoils, Including the Treatment of Irregular Shock-Wave Motions," *AIAA Paper 77-205*, Jan. 1977.
- ⁴⁴Rizzetta, D. P., "A Comparative Study of Two Computational Methods for Calculating Unsteady Transonic Flows About Oscillating Airfoils," Air Force Flight Dynamics Lab., AFFDL-TR-77-118, Dayton, OH, Nov. 1977.
- ⁴⁵Rizzetta, D. P., "The Aeroelastic Analysis of a Two-Dimensional Airfoil in Transonic Flow," Air Force Flight Dynamics Lab., AFFDL-TR-77-126, Dayton, OH, Dec. 1977.
- ⁴⁶Yang, T. Y., Striz, A. G., and Guruswamy, P., "Flutter Analysis of Two-Dimensional and Two-Degree of Freedom Airfoils in Small Disturbance Unsteady Transonic Flow," Air Force Flight Dynamics Lab., AFFDL-TR-78-202, Dayton, OH, Dec. 1978.
- ⁴⁷Tijdeman, H., van Nunen, J. W. G., Kraan, A. N., Persoon, A. J., Poestkoke, R., Roos, R., Schippers, P., and Siebert, C. M., "Transonic Wind Tunnel Tests on an Oscillating Wing with External Stores: Part I—General Description," Air Force Flight Dynamics Lab., AFFDL-TR-78-194, Dayton, OH, Dec. 1978.
- ⁴⁸Tijdeman, H., van Nunen, J. W. G., Kraan, A. N., Persoon, A. J., Poestkoke, R., Roos, R., Schippers, P., and Siebert, C. M., "Transonic Wind Tunnel Tests on an Oscillating Wing with External Stores: Part II—The Clean Wing," Air Force Flight Dynamics Lab., AFFDL-TR-78-194, March 1979.
- ⁴⁹Tijdeman, H., van Nunen, J. W. G., Kraan, A. N., Persoon, A. J., Poestkoke, R., Roos, R., Schippers, P., and Siebert, C. M., "Transonic Wind Tunnel Tests on an Oscillating Wing with External Stores: Part III—The Wing with Tip Store," Air Force Flight Dynamics Lab., AFFDL-TR-78-194, Dayton, OH, May 1979.
- ⁵⁰Tijdeman, H., van Nunen, J. W. G., Kraan, A. N., Persoon, A. J., Poestkoke, R., Roos, R., Schippers, P., and Siebert, C. M., "Transonic Wind Tunnel Tests on an Oscillating Wing with External Stores: Part IV—The Wing with Underwing Store," Air Force Flight Dynamics Lab., AFFDL-TR-78-194, Dayton, OH, Sept. 1979.
- ⁵¹Wilkinson, K., Markowitz, J., Lerner, E., Chipman, R., and George, D., "An Automated Procedure for Flutter and Strength Analysis and Optimization of Aerospace Vehicles," *Theory and Application*, Vol. I, Air Force Flight Dynamics Lab., AFFDL-TR-75-137, Dayton, OH, Dec. 1975.
- ⁵²Markowitz, J., and Isakson, G., "FASTOP-3: A Strength, Deflection, and Flutter Optimization Program for Metallic and Composite Structures," *Theory and Application*, Vol. I, Air Force Flight Dynamics Lab., AFFDL-TR-78-50, Dayton, OH, May 1978.
- ⁵³Shirk, M. H., Hertz, T. J., and Weissshaar, T. A., "Aeroelastic Tailoring: Theory, Practice, Promise," *Journal of Aircraft*, Vol. 23, No. 1, 1986, pp. 6-18.
- ⁵⁴Braymen, W. W., Rogers, W. A., and Shirk, M. H., "Wind Tunnel Test and Aerodynamic Analysis of Three Aeroelastically Tailored Wings," *Proceedings of the 13th Congress of the International Council of the Aeronautical Sciences and AIAA Aircraft Systems and Technology Conference*, Vol. 2, AIAA, New York, 1982, pp. 1243-1255.
- ⁵⁵Sherrer, V. C., Hertz, T. J., and Shirk, M. H., "Wind Tunnel Demonstration of Aeroelastic Tailoring Applied to Forward Swept Wings," *Journal of Aircraft*, Vol. 18, No. 11, 1981, pp. 976-983.
- ⁵⁶Wilkinson, K., and Rauch, F., "Predicted and Measured Divergence Speeds of an Advanced Composite Forward Swept Wing Model," Air Force Wright Aeronautical Lab., AFWAL-TR-80-3059, Dayton, OH, July 1980.
- ⁵⁷Ellis, J. W., Dobbs, S. K., and Miller, G. D., "Structural Design and Wind Tunnel Testing of a Forward Swept Fighter Wing," Air Force Wright Aeronautical Lab., AFWAL-TR-80-3073, Dayton, OH, July 1980.
- ⁵⁸Cross, A. K., and Albano, E. A., "Computer Techniques for the Rapid Flutter Clearance of Aircraft Carrying External Stores: Part I—Perturbation Theory and Applications and Part II—Documentation of Data Retrieval System and Perturbation Program," Air Force Flight Dynamics Lab., AFFDL-TR-72-114, Dayton, OH, Feb. 1973.
- ⁵⁹Ferman, M. A., "A Rapid Method for Flutter Clearance of Aircraft with External Stores," Air Force Flight Dynamics Lab., AFFDL-TR-73-74, Dayton, OH, Sept. 1973.
- ⁶⁰Ferman, M. A., "Improved Aircraft External Store Flutter Prediction, Vol. I—Theory and Application," Air Force Flight Dynamics Lab., AFFDL-TR-78-199, Dayton, OH, Dec. 1979.
- ⁶¹Triplett, W. E., Kappus, H.-P. F., and Landy, R. J., "Active Flutter Suppression Systems for Military Aircraft—A Feasibility Study," Air Force Flight Dynamics Lab., AFFDL-TR-72-116, Dayton, OH, Feb. 1973.
- ⁶²Hwang, C., Winther, B. A., and Mills, G. R., "Demonstration of Active Wing/Store Flutter Suppression Systems," Air Force Flight Dynamics Lab., AFFDL-TR-78-65, Dayton, OH, June 1978.
- ⁶³Hwang, C., Johnson, E. H., Mills, G. R., and Pi, W. S., "Additional Demonstration of Active/Store Flutter Suppression Systems," Air Force Wright Aeronautical Lab., AFWAL-TR-80-3093, Dayton, OH, Aug. 1980.
- ⁶⁴Hwang, C., Johnson, E. H., Wells, G. R., Noll, T. E., Farmer, M. G., Honlinger, H., Sensburg, O., Kuhn, M., Godel, H., Destuynder, R., and Turner, M. R., "Report on a Cooperative Programme on Active Flutter Suppression," AGARD, Rept. 689, Neuilly-Sur-Seine, France, April 1980.
- ⁶⁵Wykes, J. H., "Active Flutter Suppression of an Aeroelastically Tailored HiMAT Vehicle," Air Force Flight Dynamics Lab., AFFDL-TR-79-3012, Dayton, OH, Feb. 1979.
- ⁶⁶Peloubet, R. P., Jr., Haller, R. L., and Bolding, R. M., "F-16 Flutter Suppression System Investigation," *AIAA Paper 80-0768*, May 1980.
- ⁶⁷Reed, L. T., Gilman, J., Cooley, D. E., and Sevart, F., "A Wind Tunnel Investigation of a B-52 Model Flutter Suppression System," *AIAA Paper 74-401*, April 1974.
- ⁶⁸Rogers, R. L., Felt, L. R., and Hodges, G. E., "Active Flutter Suppression—A Flight Test Demonstration," *AIAA Paper 74-402*, April 1974.

- ⁶⁹Felt, L. R., Huttshell, L. J., Noll, T. E., and Cooley, De. E., "Aeroservoelastic Encounters," *Journal of Aircraft*, Vol. 16, No. 7, 1979, pp. 477–483.
- ⁷⁰Triplett, W. E., "A Feasibility Study Active Wing/Store Flutter Control," *Journal of Aircraft*, Vol. 9, No. 6, 1972, pp. 438–444.
- ⁷¹Peloubet, R. P., Jr., Haller, R. L., Cunningham, A. M., Cwach, E. F., and Watts, D., "Application of Three Aeroservoelastic Stability Analysis Techniques," Air Force Flight Dynamics Lab., AFFDL-TR-76-89, Dayton, OH, Sept. 1976.
- ⁷²Sallee, V. J., "ADAM 2.0: A Method for Aeroservoelastic Analysis of Aircraft with Digital Flight Control Systems, Vol. I: Theoretical Manual," Wright Research and Development Center, WRDC-TR-89-3073, Vol. I, Dayton, OH, June 1989.
- ⁷³Weisshaar, T. A., Zeiler, T. A., Hertz, T. J., and Shirk, M. H., "Flutter of Forward Swept Wings, Analysis and Tests," AIAA Paper 82-0646, May 1982.
- ⁷⁴Blair, M., and Weisshaar, T. A., "Swept Composite Wing Aeroelastic Divergence Experiments," *Journal of Aircraft*, Vol. 19, No. 11, 1982, pp. 1019–1024.
- ⁷⁵Hönlinger, H., Mussman, D., Manser, R., and Huttshell, L. J., "Development and Flight Test of an Active Flutter Suppression System for the F-4F with Stores—Part III, Flight Demonstration of the Active Flutter Suppression System," Air Force Wright Aeronautical Lab., AFWAL-TR-82-3040, Part III, Dayton, OH, June 1983.
- ⁷⁶Johnson, E. H., Hwang, C., Pi, W. S., and Harvey, C. A., "Test Demonstration of Digital Control of Wing/Store Flutter," AIAA Paper 82-0645-CP, May 1982.
- ⁷⁷Johnson, E. H., Hwang, C., Joshi, D. D., Harvey, C. A., Huttshell, L. J., and Farmer, M. B., "Adaptive Flutter Suppression—Analysis and Tests," AGARD, Paper 4, AGARD-R-703, Sept. 1982.
- ⁷⁸Peloubet, R. P., Jr., Bolding, R. M., and Penning, K. B., "Adaptive Flutter Suppression Wind Tunnel Demonstration," Air Force Wright Aeronautical Lab., AFWAL-TR-87-3053, Dayton, OH, Oct. 1987.
- ⁷⁹Pendleton, E. W., Lee, M. R., and Wasserman, L. S., "An Application of the Active Flexible Wing Concept to the Agile Falcon," *Journal of Aircraft*, Vol. 29, No. 3, 1992, pp. 444–451.
- ⁸⁰Pendleton, E., Bessette, D., Field, P., Miller, G., and Griffin, K., "Active Aeroelastic Wing Flight Research Program: Technical Program and Model Analytical Development," *Journal of Aircraft*, Vol. 37, No. 4, 2000, pp. 554–561.
- ⁸¹Triplett, W. E., "Pressure Measurements on Twin Vertical Tails in Buffeting Flow," Air Force Wright Aeronautical Lab., AFWAL-TR-82-3015, Dayton, OH, April 1982.
- ⁸²Pettit, C., Brown, D., Banford, M., and Pendleton, E., "Full-Scale Wind Tunnel Pressure Measurements of an F/A-18 Tail During Buffet," *Journal of Aircraft*, Vol. 33, No. 6, 1996, pp. 1148–1156.
- ⁸³Pendleton, E., Moster, G., and Keller, D., "Transonic Aeroelastic Models of Hypersonic Highly Swept Lifting Surfaces," *Journal of Aircraft*, Vol. 32, No. 6, 1995, pp. 1169–1176.
- ⁸⁴Ricketts, R. H., Noll, T. E., Whitlow, W. W., and Huttshell, L. J., "An Overview of Aeroelasticity Studies for the National Aero-Space Plane," AIAA Paper 93-1313, April 1993.
- ⁸⁵Borland, C. J., "XTRAN3S-Transonic Steady and Unsteady Aerodynamics for Aeroelastic Applications," Air Force Wright Aeronautical Lab., AFWAL-TR-85-3124, Dayton, OH, Jan. 1986.
- ⁸⁶Horsten, J. J., den Boer, R. G., and Zwaan, R. J., "Unsteady Transonic Pressure Measurements on a Semi-Span Wing Tunnel Model of a Transport-Type Supercritical Wing (LANN Model): Part I—General Description, Aerodynamic Coefficients, and Vibration Modes; Part II—Pressure Distributions (Plotted) and Plots of the Vibration Modes," Air Force Wright Aeronautical Lab., AFWAL-TR-83-3039, Dayton, OH, March 1983.
- ⁸⁷Cunningham, A. M., and den Boer, R. G., "Overview of Unsteady Transonic Wind Tunnel on a Semispan Straked Delta Wing Oscillating in Pitch," Wright Lab., WL-TR-94-3017, Dayton, OH, Aug. 1994.
- ⁸⁸Cunningham, A. M., den Boer, R. G., Dogger, C. S. M., Geurts, E. G. M., Retel, A. P., and Zwaan, R. J., "Unsteady Transonic Wind Tunnel Test on a Semispan Straked Delta Wing Model Oscillating in Pitch: Part I—Description of Model, Test Setup, Data Acquisition and Data Processing," Wright Lab., WL-TR-94-3094, Dayton, OH, Dec. 1994.
- ⁸⁹Cunningham, A. M., den Boer, R. G., Dogger, C. S. M., Geurts, E. G. M., Retel, A. P., and Zwaan, R. J., "Unsteady Transonic Wind Tunnel Test on a Semispan Straked Delta Wing Model Oscillating in Pitch: Part II—Selected Data Points for Harmonic Oscillation," Wright Lab., WL-TR-94-3095, Dayton, OH, June 1995.
- ⁹⁰Cunningham, A. M., den Boer, R. G., Dogger, C. S. M., Geurts, E. G. M., Retel, A. P., and Zwaan, R. J., "Unsteady Transonic Wind Tunnel Test on a Semispan Straked Delta Wing Model Oscillating in Pitch: Part III—Selected Data Points for Simulated Maneuvers," Wright Lab., WL-TR-94-3096, Dayton, OH, Nov. 1995.
- ⁹¹"Verification and Validation Data for Computational Unsteady Aerodynamics," Research and Technology Organization, RTO TR 26, St. Joseph Ottawa/Hall, Quebec, Canada, Oct. 2000.
- ⁹²Schuster, D., Vadyak, J., and Atta, E., "Static Aeroelastic Analysis of Fighter Aircraft Using a Three-Dimensional Navier–Stokes Algorithm," *Journal of Aircraft*, Vol. 27, No. 9, 1990, pp. 820–825.
- ⁹³Smith, M. J., Schuster, D. M., Huttshell, L. J., and Buxton, B., "Development of an Euler/Navier–Stokes Aeroelastic Method for Three-Dimensional Vehicles with Multiple Flexible Surfaces," AIAA Paper 96-1513-CP, April 1996.
- ⁹⁴Johnson, E. H., and Venkayya, V. B., "Automated Structural Optimization System (ASTROS), Theoretical Manual," Air Force Wright Aeronautical Lab., AFWAL-TR-88-3028, Dayton, OH, Vol. I, Dec. 1988.